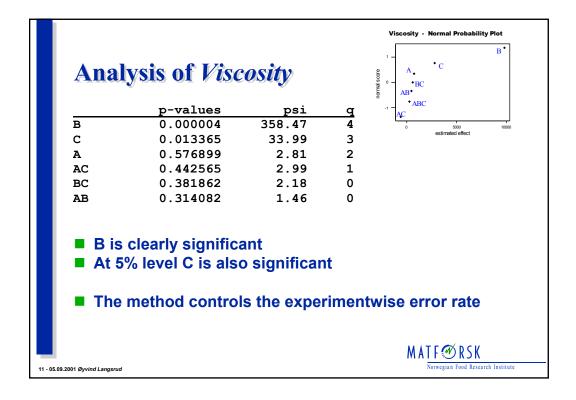
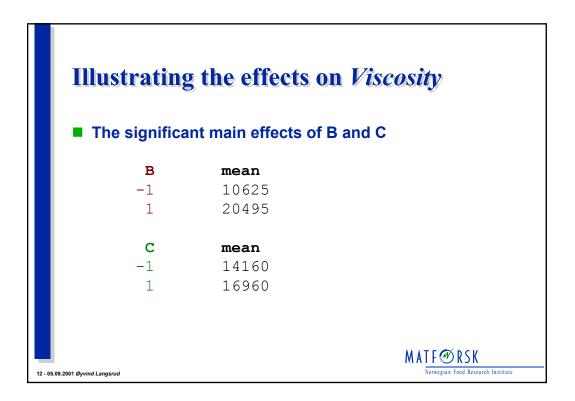
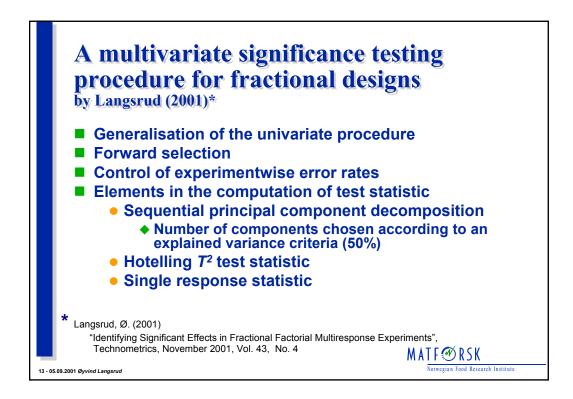
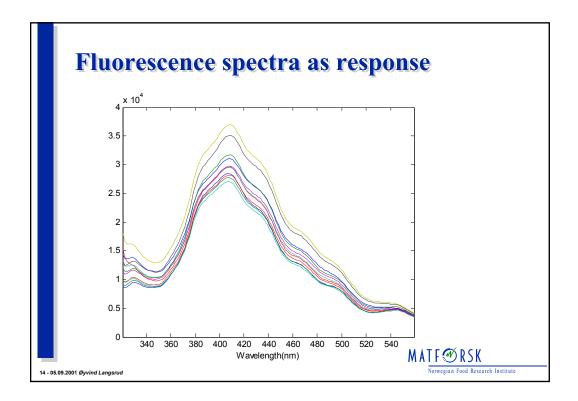


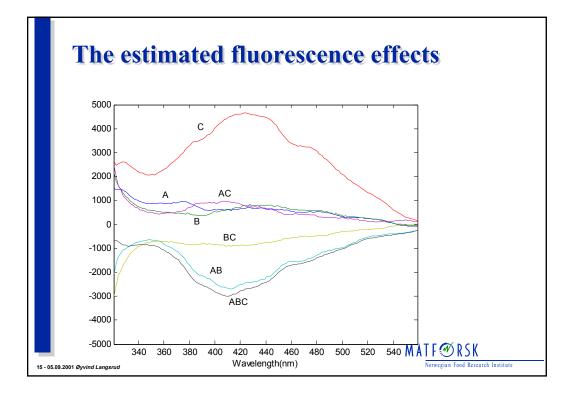
	lysis of <i>Sta</i> ard selection (Langs	· · · · · · · · · · · · · · · · · · ·	, 1998)	$ \begin{array}{c} B \\ B \\ B \\ B \\ B \\ B \\ C \end{array} $
	p-values	psi	q	BC
С	0.466105	4.91	4	-1 0 1 estimated effect
в	0.540302	3.75	3	
BC	0.504727	3.39	2	
AB	0.935020	0.34	1	
А	0.948044	0.09	0	
AC	0.788238	0.09	0	
An	e largest (absolu "F-statistic" wh q smallest effe	nere the d		ator contains







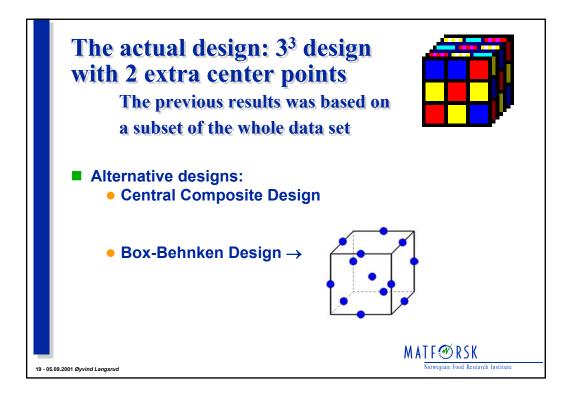




	p-values	psi	m	q	expl.var.
С	0.170449	9.93	1	4	0.9679
AB	0.729027	2.37	1	3	0.9441
BC	0.963883	0.45	1	2	0.9285
A	0.950417	0.28	1	1	0.9444
AC	0.879826	0.21	1	0	0.9602
в	0.703025	0.18	1	0	0.9744
test	the number of pr ing <i>l.var.</i> is the varian ponents.	-			

	k	1	149-					
	neo	logy	as multiv	aria	te res	pons		
	_						_	
y-s	hear-s	stress,Pa	y-Viscosity, Pa-s		r-stress,Pa		se, degree	s-G*,Pa
		3.610	37.375		1.645		25.355	44.820
	3.610		35.515		1.345		26.490	51.010
	7.105		160.320		3.910		22.160	74.130
	7.105		154.175		4.055		20.960	102.530
	5.940		121.835		1.045		24.700	59.585
	5.940		57.835		1.040		25.405	64.365
	7.105		183.665		4.695		19.845	126.835
	7.105		166.020		3.660		20.120	138.610
	5.940		98.355		2.700		22.670	78.595
		5.940	93.525		2.575		23.550	71.030
		5.940	138.325		2.575		23.320	71.665
s-G	`,Pa	s-G",Pa	f-Phase, degree	f-G*,Pa	f-G`,Pa	f-G",Pa	f-lutn-0	3`
40	.510	19.180	24.210	48.090	43.870	19.685	0.27	70
45	. 650	22.740	25.055	52.375	47.460	22.095	0.28	35
69	.075	26.695	17.145	111.860	106.875	32.975	0.19	95
95	.770	36.585	18.850	114.585	108.435	37.020	0.21	10
54	.155	24.815	24.180	60.925	55.705	24.540	0.26	60
58	.185	27.485	23.905	68.435	62.570	27.715	0.26	50
119	. 320	42.990	18.315	142.310	135.090	44.680	0.21	10
130	.315	47.050	18.410	153.410	145.650	47.985	0.21	15
72	.560	30.175	21.005	85.195	79.555	30.465	0.24	40
65	.135	28.310	20.595	87.630	82.025	30.815	ΓΓ 🕢 🕫 🌠	35
65	.825	28.310	21.435	81.745	76.105	29.830	IF ∭ K⊖ K	45
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	p-values	psi	m	q	expl.var.
В	0.000001	1013.53	1	<u> </u>	0.8895
2	0.011701	36.24	1	3	0.5663
BC	0.008968	45.36	1	2	
A	0.000349	287.58	1	1	0.5592
AC	0.155988	6.02	1	0	0.5410
AB	0.398106	4.55	2	0	0.8017

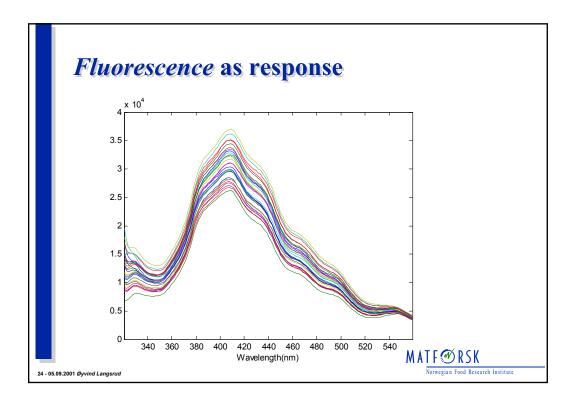


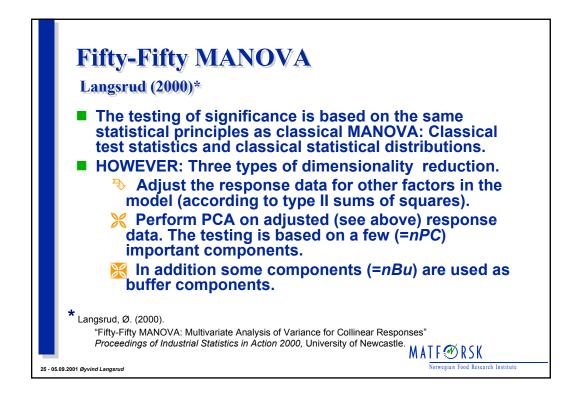
	T 7- A		•	• •	7.9	• 4	
	JVA	analy	SIS 01		ISCOS	lty 🛛	
3 1 i			•• • • • • • • •			1 00 5-	
Analysi	s or vai	riance for V	/iscosit,	us	ing Adjust	ed SS IO	r Tests
Source	DF	Seq SS	Adj S	s	Adj MS	F	P
A	2	5210297	532040	7	2660204	5.40	0.026
в	2	413321269	41328715	6	206643578	419.10	0.000
с	2	46398397	4641018	5	23205093	47.06	0.000
A*B	4	1868745	186847	6	467119	0.95	0.476
A*C	4	6397751	640735	3	1601838	3.25	0.060
B*C	4	7677944	767794	4	1919486	3.89	0.037
Error	10	4930680	493068	0	493068		
Total	28	485805083					
			в	* c	Mean	SE Mean	
				-1		405.4	
			-1	0	10500	405.4	
Least Squar	es Means	for Viscosit	-1	1	11893	405.4	
_			0	-1	14560	405.4	
A -1	Mean 15153	SE Mean 234.1	0	0	15553	344.7	
-1	15155	223.0	0	-	10010	405.4	
ů 1	16016	234.1	1	-		405.4	
_			1	0		405.4	
			1	1	22687	405.4	
						٨	∧ A T F 𝒇 R S K
						l l	AATE 🖤 KON

<section-header>Unbalanced blocks (days) → <u> Modified analysis</u> • Continuos instead of categorical sariables (second order model) • Unbalanced analysis • Use Type II Instead of Type III sums of Squares • Report sums of squares as the fraction of the total sums of squares (explained variance)</section-header>	λ B C Day -1 -1 -1 4 0 -1 -1 5 1 -1 -1 3 0 0 -1 3 0 0 -1 3 -1 1 -1 4 0 1 -1 4 1 1 -1 4 0 1 -1 4 0 1 -1 4 0 -1 0 2 -1 0 0 1 0 0 1 1 0 0 0 1 0 0 1 1 0 1 1 1 0 1 1 1 0 0 1 1 0 1 1 1 0 1 1 1
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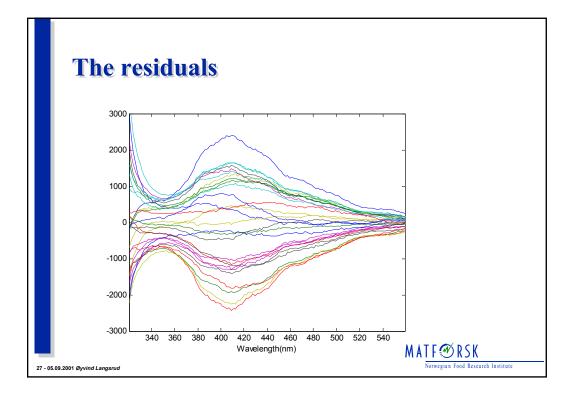
	Stal	bility			
	Source	DF	exVarSS	p-Value	
	A	1	0.004334	0.586609	
	A*A	1	0.001639	0.737202	
	в	1	0.217732	0.001466	
	B*B	1	0.001558	0.743540	
	С	1	0.291266	0.000443	
	C*C	1	0.004434	0.582350	
	A*B	1	0.019144	0.261604	
	A*C	1	0.003016	0.649536	
	B*C	1	0.026667	0.189030	
	Block	4	0.037545	0.622876	
	Error	14	0.195853		
				С	adjusted mean
	в	adius	ted mean	-1	7.0351
	_	-		-	0 4511
	-1	7.1	342	1	8.4511
	1	8.3	874		
					M AT F @ RSK
	I				
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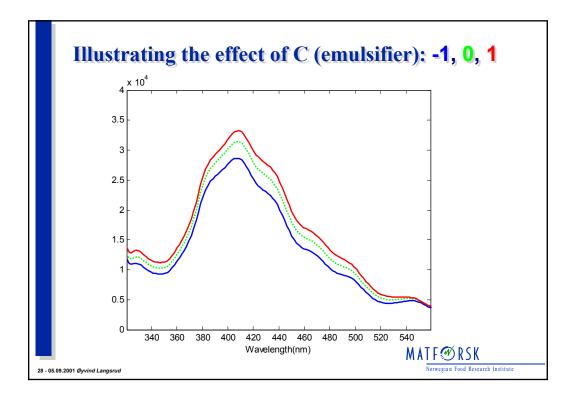
T- 74	•.			
Visco	osity			
Source	DF	exVarSS	p-Value	
A	1	0.00004	0.945192	
A*A	1	0.010226	0.004367	
В	1	0.746661	0.00000	
B*B	1	0.000065	0.793518	
С	1	0.086138	0.00000	
C*C	1	0.000417	0.508874	
A*B	1	0.003133	0.083323	
A*C	1	0.000131	0.709347	
B*C	1	0.003740	0.060808	
Block	4	0.018681	^{0.008292} C	adj. mean
Error	15	0.013652	C	-
			-1	13811
			1	17089
A	adj. me	ean	T	17089
-1	15822			
0	14692	В	adj. m	nean
1	15799	-1	10177	
		1	20580	M A T F 🕐 R S K
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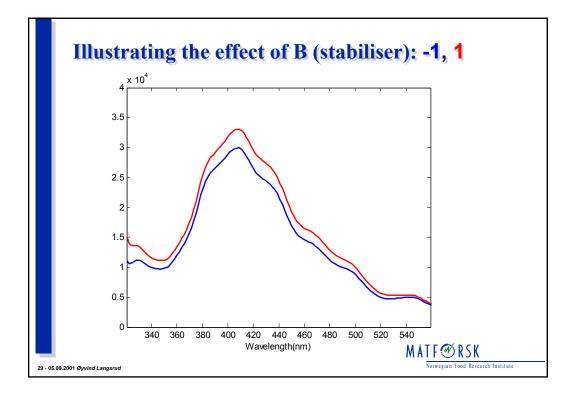


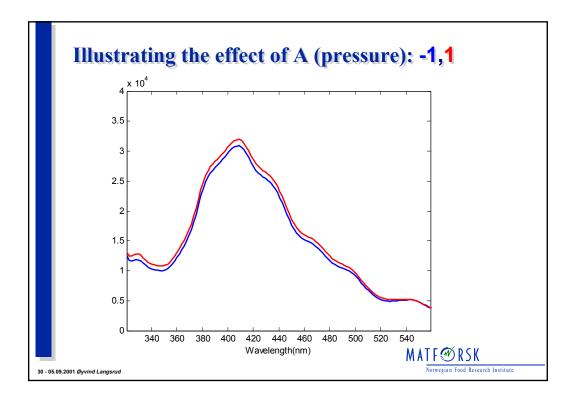


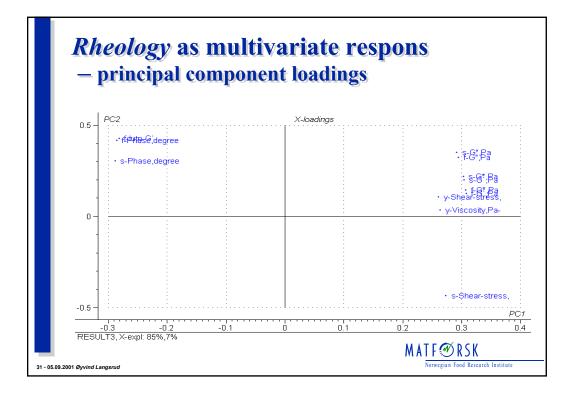
NOTE: Due	to missir	ng values, 1	obse	rvat	tion was	removed	
		-	RSION			28 respon	ses
Source	DF	exVarSS	nPC	nBu		exVarBU	p-Value
A	1	0.017874	1	5	0.949	1.000	0.029414
A*A	1	0.017322	1	5	0.948	1.000	0.219138
В	1	0.139253	1	5	0.966	1.000	0.001664
B*B	1	0.027987	1	5	0.955	1.000	0.237324
с	1	0.323186	1	5	0.973	1.000	0.000002
C*C	1	0.004042	1	5	0.947	1.000	0.596164
A*B	1	0.009311	1	5	0.950	1.000	0.396251
A*C	1	0.006879	1	5	0.921	1.000	0.670535
B*C	1	0.011193	1	5	0.937	1.000	0.366550
Block	4	0.221358	1	5	0.962	1.000	0.009285
Error	14	0.183920	- ST	AND	ARDIZATI	ON OFF	

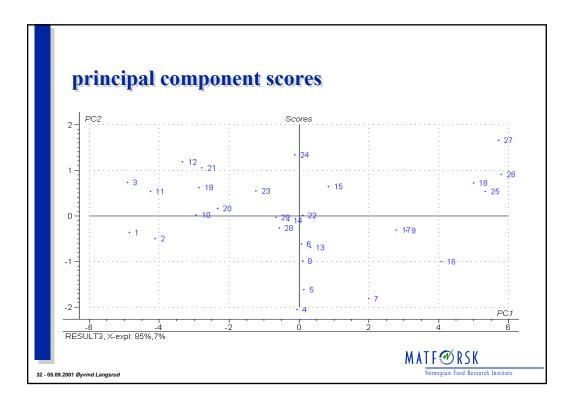












Analysis of *Rheology*

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	FIFTY-FIFTY	MANOVA VEI	RSION	11.1	1	2 respons	es
Sourc	e DF	exVarSS	nPC	nBu	exVarPC	exVarBU	p-Value
A	1	0.024601	2	5	0.685	0.997	0.000002
A*A	1	0.019789	2	5	0.790	0.996	0.005452
в	1	0.671111	1	5	0.947	0.999	0.00000
B*B	1	0.011262	2	5	0.718	0.993	0.235250
С	1	0.082027	2	5	0.763	0.998	0.00000
C*C	1	0.014066	2	5	0.754	0.996	0.197659
A*B	1	0.007798	2	5	0.753	0.996	0.037500
A*C	1	0.003366	2	5	0.771	0.995	0.154337
B*C	1	0.014732	2	5	0.722	0.996	0.000064
Block	c 4	0.046025	2	5	0.836	0.995	0.060237
Error	: 15	0.064372	- S1	'ANDA	RDIZATI	ON ON	
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